

# Femtosecond Laser Inscribed Small-Period Long-Period Fiber Gratings With Dual-Parameter Sensing

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**Abstract**—A small-period long-period grating (LPG) with a period of  $40\mu\text{m}$  fabricated in a single-mode fiber by femtosecond laser direct writing has been demonstrated. A series of high-order Bragg resonant peaks of Bragg grating and attenuation bands of LPG can be observed simultaneously in the broadband spectrum range that exhibited different responses to surrounding refractive index, temperature, and axial strain. Meanwhile, we provided a sensitivity matrix to correct the errors caused by temperature in measurements of refractive index and strain to achieve a dual-parameter fiber sensor at high temperature.

**Index Terms**—Fiber optic sensors, femtosecond laser direct writing, small-period long-period fiber gratings.

## I. INTRODUCTION

OPTIC fiber sensors have widely attracted great attention in the past few decades due to their advantages of small size, anti-electromagnetic interference and corrosion resistance [1]–[3]. In real environment, there are many physical factors acting on the sensing fiber, such as strain, temperature, bending, twisting, refractive index (RI) and so on. The signal from the fiber sensing area is actually subjected to the effects of multiple physical factors, therefore, the parameter to be measured cannot be accurately measured. Temperature and strain cross-sensitivity is one of the primary causes of errors associated with practical application of fiber sensors [4]. Therefore, the multi-parameter simultaneous monitoring of optic fiber sensors is of great significance.

Many methods have been proposed to solve cross-sensitivity problem including combination of fiber Bragg gratings (FBG) and long-period gratings (LPG) [5]–[6], reference grating methods and extraordinary designs of fiber material, structure and package [7]–[10]. These solutions are effective in

compensating cross-sensitivity. However, the introduction of additional grating structures increases the fabrication cost and complexity. Special designs of sensing units, such as coating suitable polymer materials on the fiber surface or employing core materials with different refractive index, might reduce the thermal stability, mechanical strength and sensitivity of the sensor.

To overcome these problems, we proposed an optical fiber sensor based on small-period long-period grating (SP-LPGs). In the experiment, we found that when the grating period is tens of microns can cause light coupling not only between the forward and backward core mode but between the forward core mode and cladding modes. Before, Shen *et al.* reported a UV inscribed small-period ( $25\mu\text{m}$ ) long-period grating with unique polarization-dependent dual-peak pairs [11], in which, the 47th-order Bragg resonant peak can be observed. In this letter, a compact SP-LPG with the period of  $40\mu\text{m}$  fabricated by femtosecond laser direct writing (FsLDW) is proposed. FsLDW is a 3D laser processing technology with high spatial resolution [12]–[13], we can precisely control the laser processing area size, shape and direction, and the fabrication process has a high repeatability due to the program control [14], [15]. Based on this method, we can realize strong RI modulation pattern in the fiber core to overcome the weak average RI modulation caused by small duty cycle in the large grating period. We fabricated a grating with short length and the Bragg reflection peaks and attenuation bands of long-period grating both appear in the spectrum. In addition, the sensing abilities of the SP-LPGs for environmental RI, temperature and axial strain have been investigated.

## II. EXPERIMENTS

In the experiment, direct writing of the SP-LPG in standard single-mode fiber (Corning SMF-28) with infrared fs laser pulses was realized with a Ti: sapphire regenerative amplifier laser system (Spectra Physics) operating at 800 nm. The pulse duration and the maximum repetition frequency were 100 fs and 2.5 kHz. The laser beam with pulse energy of 70 nJ was focused into the fiber by an oil immersed  $60\times$  Olympus objective (N.A., 1.42). The fiber was set on a computer-controlled 3D translation platform with a motion spatial resolution of 20 nm. The overall translation velocity of the fiber was set at  $10\mu\text{m/s}$  during the fabrication process. After the inscription, the grating region was annealed at  $120^\circ\text{C}$

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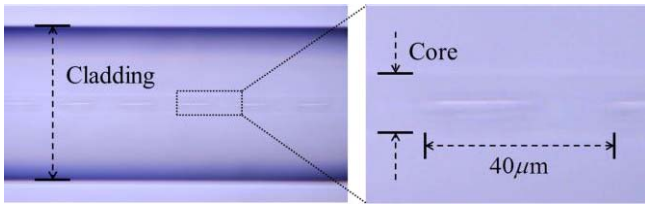


Fig. 1. Microscopic images of femtosecond laser inscribed SP-LPG with period of  $40\mu\text{m}$ .

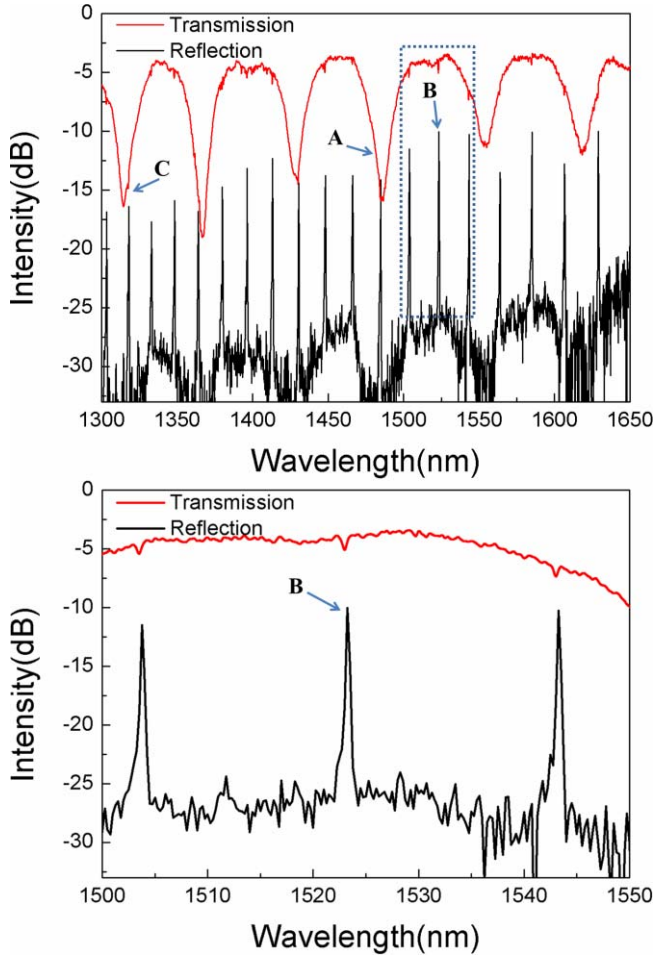


Fig. 2. (a) Transmission and reflection spectra of the SP-LPG. (b) Zoomed-in spectrum around  $1523\text{nm}$ , where some small dips corresponding to Bragg resonant peaks can be seen.

for 24h to stabilize the structure. Fig. 1(a) shows the structure of the fabricated SP-LPG with the period of  $40\mu\text{m}$  and a duty cycle of 0.5. The period number is 75 and the grating length is only 3 mm. The micrograph exhibits that the periodic straight-line RI modulation region along the fiber axis is located in the center of fiber core.

Both the Bragg resonant peaks and attenuation band of the SP-LPG can be clearly observed from 1300 nm to 1650 nm in Fig. 2(a). The side-mode suppression ratio (SMSR) of the strongest Bragg resonant wavelength  $\lambda_B$  at  $1522.8\text{ nm}$  was  $\sim 17\text{ dB}$  with a full width at half maximum (FWHM) of  $\sim 0.4\text{ nm}$ . Three small dips in transmission corresponding to Bragg resonant wavelength including  $\lambda_B$  can be seen in Fig. 2(b). Generally, a longer grating length can enhance the

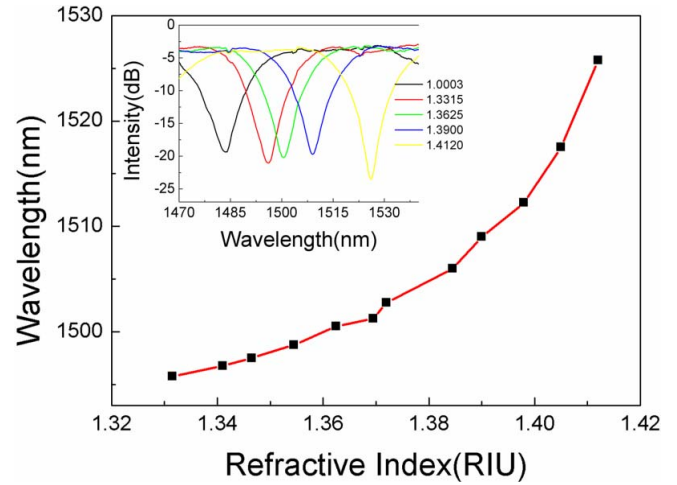


Fig. 3. Relationship between resonant dip wavelength and the surrounding RI. The inset shows the evolution of the transmission spectrum versus to the increasing RI of the surrounding liquid.

Bragg reflectivity and the attenuation dips will become sharper, which helps to improve the resolution of the sensor [16]. However, in our experiment we found that the attenuation dips of LPG will get weak with an excessive increase of number of grating period. So we set the number of grating period and length of the grating to 75 and 3mm to achieve a good performance.

### III. SENSING CHARACTERISTICS AND DISCUSSION

After the fabrication, we studied the sensing characteristics of the SP-LPGs, SP-LPG was connected by a broadband light source (Superk Compact, NKT Photonics) and an optical spectrum analyzer (OSA) (AQ6370B, Yokogawa) during the testing process. The transmitted signal and the reflected signal was collected by OSA respectively. The symbol A in Fig. 2(a) corresponds to the attenuation dip in RI measurement. The symbol B and C correspond to the Bragg resonant peak and attenuation dip in temperature and strain measurement. In the experiment, a series of glycerin-water mixed solution with RI range from 1.3315 to 1.4120 was applied in turn to the SP-LPG sensor. The SP-LPG was cleaned in ethanol and deionized water after each measurement to remove the residual chemical from the grating and to recover the original spectrum [17]. Fig.3 shows the resonant wavelength shift of the SP-LPG with different RI. The inset of Fig. 3 shows that the wavelength  $\lambda_A$  exhibited redshift characteristics as the RI increasing in the range of 1.3315–1.4120. The main figure shows that is a non-linear relationship and the shift becomes faster when the RI is close to 1.4120. The average sensitivities of  $\lambda_A$  in the RI range of 1.3315–1.3845 and 1.3845–1.4050 are about  $189.8\text{ nm/RIU}$  and  $542.8\text{ nm/RIU}$ , respectively. The sensitivity reaches as maximum as  $1178.6\text{ nm/RIU}$  in the RI range of 1.4050–1.412.

Besides to the surrounding RI, the temperature and axial strain responses of the SP-LPG were also investigated. Placing the fiber in a tube furnace, temperature was increased from room temperature ( $24\text{ }^\circ\text{C}$ ) to  $900\text{ }^\circ\text{C}$  with an increment

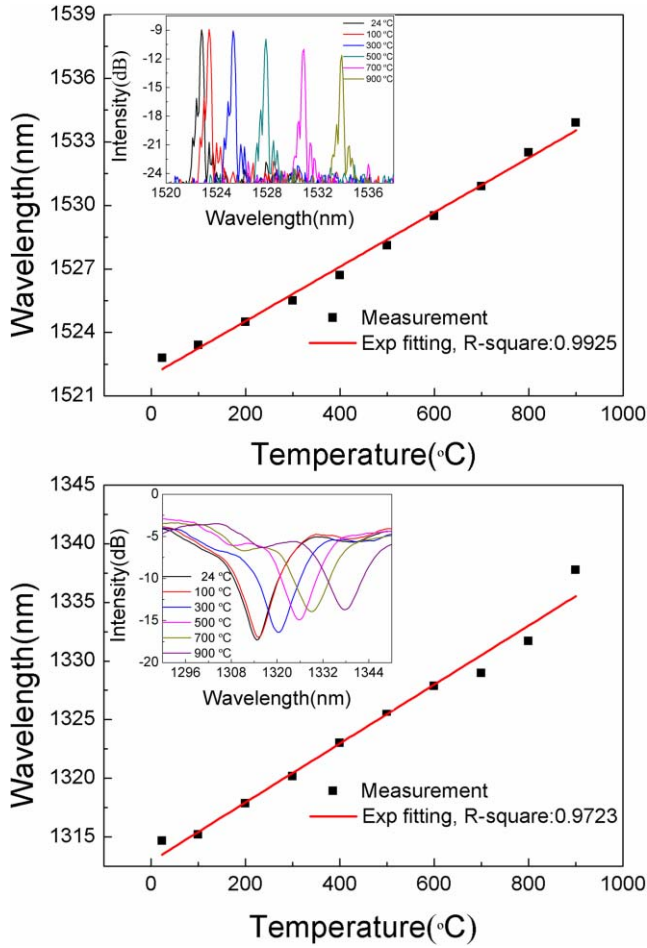


Fig. 4. (a) Relationship between Bragg resonant wavelength and the temperature. The inset shows the evolution of the reflection spectrum versus to temperature. (b) Relationship between resonant dip wavelength and the temperature. The inset shows the evolution of the transmission spectrum versus to temperature.

of 100 °C and the holding time at each temperature point is 10 minutes that is long enough for the stabilization of spectrum and recording the data. Fig. 4(a) shows the temperature response of the 76th-order Bragg resonant  $\lambda_B$  at 1522.8 nm. As shown in the figure, the Bragg resonant peak showed an obvious redshift with the temperature increasing. The relationship between wavelength shift of the resonant peak and temperature is linear, which shows a sensitivity of 12.85 pm/°C. As shown in Fig. 4(b), the cladding mode attenuation dip wavelength  $\lambda_C$  at 1315 nm has a linear redshift with temperature increasing. Its temperature sensitivity is 25.13 pm/°C.

As shown in Fig.5 (a), the measurement of strain response was realized by adding axial tension to the SP-LPG through a piezoelectric tensometer. The axial strain applied to the fiber could be calculated by equation [18],

$$\varepsilon = F/\pi r^2 E \quad (1)$$

where  $F$  is the axial tension,  $r$  is the cladding radius, and  $E$  is Young's modulus of silica. In the range from 0  $\mu\varepsilon$  to 1400  $\mu\varepsilon$ , the relationship between Bragg resonant wavelength  $\lambda_B$  and axial strain is linear, which shows a sensitivity of 1.21 pm/ $\mu\varepsilon$ . Fig. 5(b) shows the cladding mode attenuation

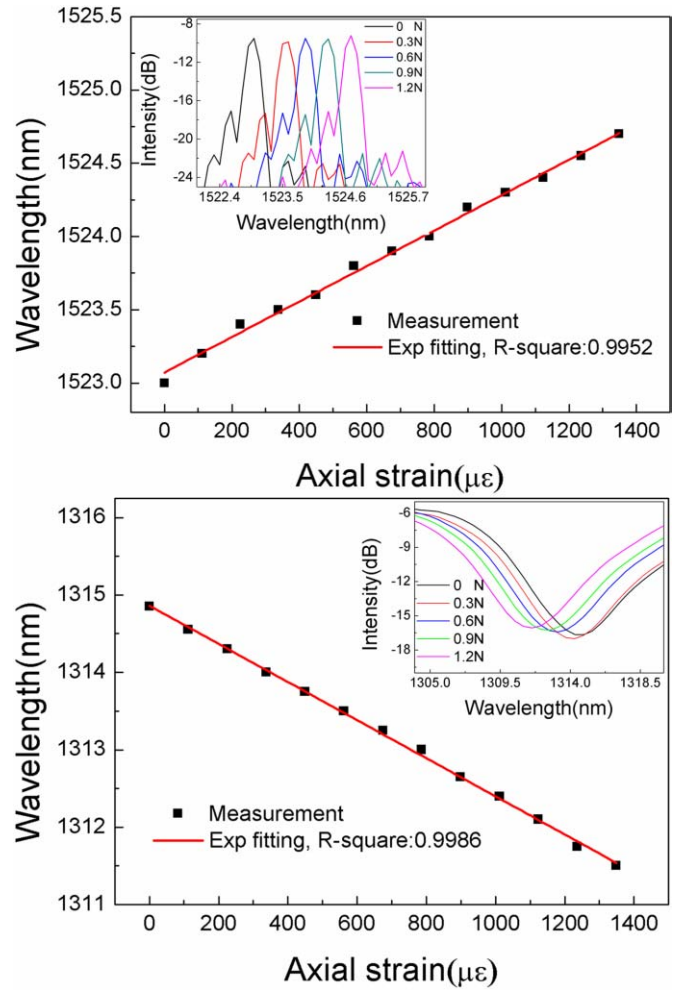


Fig. 5. (a) Relationship between Bragg resonant wavelength and the axial strain. The inset shows the evolution of the reflection spectrum versus to tension. (b) Relationship between resonant dip wavelength and the axial strain. The inset shows the evolution of the transmission spectrum versus to tension.

dip wavelength  $\lambda_C$  changing with axial strain increasing, exhibiting a negative strain sensitivity of  $-2.46$  pm/ $\mu\varepsilon$ .

Finally, we offered a sensitivity matrix to compensate the error of the cross-sensitivity in the temperature and strain measurement [19]. The relationship between wavelength shifts  $\Delta\lambda_B$ ,  $\Delta\lambda_C$  and temperature and strain changes  $\Delta T$ ,  $\Delta\varepsilon$  can be written as,

$$\begin{bmatrix} \Delta\lambda_B \\ \Delta\lambda_C \end{bmatrix} = \begin{bmatrix} K_{T1} & K_{\varepsilon1} \\ K_{T2} & K_{\varepsilon2} \end{bmatrix} \begin{bmatrix} \Delta T \\ \Delta\varepsilon \end{bmatrix}$$

where  $K_{T1}$  and  $K_{T2}$  are the temperature sensitivities of the Bragg resonant peak and LPG resonant minima, respectively.  $K_{\varepsilon1}$  and  $K_{\varepsilon2}$  are their strain sensitivities. Substituting the values obtained from experiments into the matrix, the final expression can be written as,

$$\begin{bmatrix} \Delta T \\ \Delta\varepsilon \end{bmatrix} = \begin{bmatrix} 12.85 & 1.21 \\ 25.13 & -2.46 \end{bmatrix}^{-1} \begin{bmatrix} \Delta\lambda_B \\ \Delta\lambda_C \end{bmatrix}$$

Thus, one can simultaneously obtain the changes of the temperature and the strain when the wavelength changes of the Bragg reflection peak and LPG resonant minima are determined. Similarly, the simultaneous measurement of RI and temperature can also be achieved by this method.



## IV. CONCLUSION

In summary, we experimentally demonstrated a dual-parameter fiber grating sensor based on SP-LPG fabricated by FsLDW. The fabricated SP-LPG with the period of 40  $\mu\text{m}$  shows a series of Bragg resonant peaks and LPG attenuation bands simultaneously. This grating, as one structure, has both FBG and LPFG sensing characteristics, monitoring temperature, strain, RI three parameters. We provided a sensitivity matrix to compensate the error of the cross-sensitivity in the RI and strain measurement under high temperature. Therefore, the proposed sensor can be used for sensing of dual-parameters in high temperature environment. The reduction of the length of the grating also greatly reduces the interference caused by bending in the sensing application and has a great advantage for the small integration of passive optics [20]. This SP-LPG sensor based on FsLDW has the advantages of simple fabrication process, dual-parameter sensing ability and compact size. The SP-LPG is expected to have great practical value in liquefied petroleum gas sensing [21].

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