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Highly efficient and mechanically robust stretchable polymer solar cells with random buckling



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1. Introduction

Stretchable electronics are a type of mechanically robust electronics represented by next-generation wearable and implantable devices which can be bended, folded, crumpled and stretched [1–5]. In order to facilitate the application of these modern stretchable electronic devices, the highly efficient and stretchable polymer solar cells (PSCs) are one of the best candidates for supplying energy to stretchable electronic devices [6,7]. Construction of common PSCs mainly consists of transparent electrodes, transport layers and absorption layer. For intrinsically stretchable devices, all functional layers must be elastic. However, It has been demonstrated that polymer-fullerene derivative active material films commonly used in PSCs have an elongation at break of only 0.3% [8], so that the intrinsically stretchable PSCs have not been successfully fabricated by far. To overcome the limit of the low ultimate strain of the polymer-fullerene derivative films, mechanical buckling on a rigid film has been developed by applying compressive strain to a pre-stretched elastomeric substrate. Stretchable PSCs based on the mechanical buckling by fabricating the PSCs on a pre-stretched poly(dimethylsiloxane) (PDMS)

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ABSTRACT

Stretchable polymer solar cells have shown great potential as stretchable power generators for applications in stretchable electronics, such as wearable electronics, electronic skins and stretchable displays. However, their mechanical stability and power conversion efficiency (PCE) thus are still far below the requirement for the practical applications. Here, we have developed highly efficient and stretchable polymer solar cells (PSCs) based on a random buckling process. The stretchable PSCs are fabricated by attaching the ultrathin PSC onto a pre-stretched elastomeric substrate and then releasing the prestrain to form random bucklings. Its PCE of 5.8% under 70% tensile strain is the largest to date among the reported PSCs. The stretchable PSCs exhibit small fluctuations in performance after 400 stretching-releasing cycles. This is an important step towards producing stretchable PSCs for commercial applications.

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elastomer have be demonstrated [9]. However, its strain of 22.2% and PCE of 2.0% were not sufficient to meet the demand of practical applications. Siegfried Bauer et al. presented a stretchable PSCs by fabricating the PSC on an ultrathin PET substrate and attaching it to a pre-stretched adhesive tape to form random buckles [10]. The maximal tensile strain was improved to 400% successfully, and the energy conversion efficiency of 4.0% has been achieved. However, its 22 stretching-releasing cycles was not sufficient for practical applications. The damage to the electrodes of the ultrathin PSCs during the stretching-releasing process caused by its direct contact with adhesive tape is one of the possible reasons for the low mechanical stability. So far, high efficiency and mechanical stability are still challenges for the stretchable PSCs.

On the other hand, flexible transparent conductive electrodes (TCEs) is one of the limitations for the efficient stretchable PSCs. Excellent ductility, high transmittance and conductivity are required for flexible TCEs. Traditional indium tin oxide (ITO) electrode is too friable to be suitable for highly flexible TCEs. Poly(3,4-ethylenedioxythiophene):poly(styrenesulfonate) (PEDOT:PSS) has been used in stretchable PSCs as the flexible TCEs, while its sheet resistances (RS) is higher than metallic electrodes by one order of magnitude [9,10]. Recently, ultrathin metallic TCEs fabricated on metal oxide layer such as WO₃, MoO₃, ZnO with high ductility, transmittance and conductivity are realized and they meet the requirements of the electrodes in the flexible optoelectronic devices





TCEs [11–14].

In this work, we demonstrate highly stretchable PSCs with high efficiency and improved mechanical robustness. The PSCs with an ultrathin flexible metallic TCEs were fabricated on an ultrathin photopolymer film and then attached to elastomeric support to form random bucklings. The mechanical stability has been improved by inserting a sacrificial layer between the ultrathin PSC and elastomeric support to avoid their direct contact. The stretchable PSCs exhibit power conversion efficiency of 5.8% under 70% tensile strain state, which is the highest PCE reported to date for the stretchable PSCs to the best of our knowledge. More importantly, the stretchable PSCs exhibit only small fluctuations in performance after 400 stretching-releasing cycles. This simple and low-cost method is compatible with most PCSs fabrication processes, such as thermal evaporation, spin coating, and ink-jet printing, so that it could be applied to more efficient solar cells with complex structures.

2. Experiment details

The pre-cleaned Si substrate was treated with Octadecyltrichlorosilane (OTS) [15] to realize a hydrophobic surface with lowered surface energy, so that the ultrathin PSCs can be peeled off from the substrate completely. The ultrathin photopolymer film (NOA63, Norland Inc.) was spin-coated onto the Si substrate at 12,000 rpm for 90 s and then exposed to an ultraviolet light source for 5 min with a power of 125 W. The thickness of the NOA63 film used as ultrathin flexible substrate was about 2.7 μ m. Thicknesses of the NOA63 film were measured using an XP-2 stylus profilometer (Ambios Technology, Inc.). The ultrathin anode composed of a wetting layer of 3 nm MoO₃, a seed layer of 1 nm Au, a middle layer of 7 nm Ag and a hole transport layer of 10 nm MoO₃ was deposited on the ultrathin polymer substrate by thermal evaporation in sequence at a vacuum of $<5 \times 10^{-4}$ Pa. The transmission spectra and the sheet resistance of the TCEs were measured by a UV–Vis spectrophotometer (UV-2550, SHIMADZU Co.Inc.) and a four-probe meter, respectively. The SEM images were characterized by a field emission scanning electron microscope (SEM, ISM-7500F, IEOL).

Architecture illustration of ultrathin PSC and schematic illustration of the fabrication process of stretchable PSCs are shown in Fig. 1. The PSCs were fabricated on ultrathin flexible metallic TCEs. First, a solution of PCDTBT and PC71BM (1:4 w/w, polymer concentration of 25 mg/mL) in 1,2-dichlorobenzene was spin-coated on top of the TCE at 3000 rpm for 30 s as the photoactive blend layer. The resulting layer with a thickness of about 80 nm was annealed on a hotplate at 70 °C for 1 h in the glove box. Then, a cathode of 1 nm LiF, 1 nm Al, 80 nm Ag were thermally deposited on PCDTBT:PC71BM film. Finally, a NPB film with a thickness of 0, 10, 20,30 and 40 nm was coated on the cathode as a sacrifaced layer. Two rigid plastic tapes were adhered to the two opposite sides of the adhesive elastomer (3M VHB 4905) where the distance between the two rigid tapes was exactly 5 mm. The elastomeric substrate was stretched until the distance between the two rigid tapes reached 15 mm by a home-made moving stage. The ultrathin PSC that was peeled off completely from the Si substrate was adhered onto the pre-stretched elastomeric substrate between the two rigid tapes by contacting with NPB sacrificial layer. The active area of the cell was roughly $3 \times 1.5 \text{ mm}^2$, and we aligned the long dimension of devices in the direction of stretching. We defined the length of the device to be L, so the maximum value of $L(L_{max})$ was 3 mm. We released stress by moving the rigid tapes closer together, allowing the elastomeric substrate to relax, which compressed the



Fig. 1. Schematic illustration of the fabrication process of stretchable PSCs.



Fig. 2. (a) Transmittance spectra and sheet resistance of the ultrathin flexible TCEs with and without 1 nm Au seed layer. (b) SEM images of the ultrathin flexible TCEs with and without the 1 nm Au seed layer.

device area. When the distance between the two rigid delimiters was 5 mm, the length of devices was L_0 (1.75 mm). Tensile strain was defined to be $(L - L_0)/L_0$, so the maximal tensile strain was about 70%. The photographs of the stretchable devices at 0%, 20%, 50% and 70% strain were taken by a digital single lens reflex camera. Electrical contact was made with copper wires and drops of eutectic gallium-indium at the point where the anode and cathode of the PSCs extended out of the active region of the devices. The PSCs were characterized under illumination of a solar simulator (A.M. 1.5 Global spectrum with a light intensity of 100 mW cm⁻²). All I-V characteristics were recorded using a Keithley 2400 source meter.

3. Results and discussions

Highly flexible TCEs are required for the stretchable PSCs. Here we chose ultrathin metallic TCE on ultrathin polymer film to replace the commonly-used PEDOT:PSS electrode. The construction of our TCE is MoO₃ (3 nm)/Au (1 nm)/Ag (7 nm)/MoO₃ (10 nm)). A wetting layer of 3 nm MoO₃ and a seed layer of 1 nm Au are usually placed underneath the Ag film to promote the formation of a continuous film below 10 nm. The later MoO₃ layer with a thickness of 10 nm is used both as an anti-reflective layer and a hole transport layer. Fig. 2(a) shows the transmittance spectra of the ultrathin flexible metallic TCEs with and without the Au seed layer. The transmittance can be increased from an average value of 65%-72% by introducing the Au seed layer and it is comparable with the PEDOT:PSS electrode.While the sheet resistance of the ultrathin flexible metallic TCE is decreased from 30 Ω/\Box to 7 Ω/\Box , which is one order of magnitude lower than the PEDOT:PSS electrodes at the same transmittance [16,17]. Top-view scanning electron microscope (SEM) images of the Ag films with and without the Au seed layer are shown in Fig. 2(b). It can be seen that the Ag film with the Au seed layer is more continuous, which results in the lower sheet resistance. Moreover, the more continuous film can reduce light scattering and contribute to the higher transmittance.

Polymer-fullerene derivative PCDTBT:PC₇₁BM with a high efficiency was used as the absorber layer in the stretchable PSCs. LiF/AI is used as the interfacial modification layer of cathode to match the energy level of PC₇₁BM. We used Ag layer with better ductility as cathode to replace the commonly used Al cathode. A sacrificial layer of NPB covers over the whole sample. The real photographs of the stretchable PSCs at different tensile strains are shown in Fig. 3(a).



Fig. 4. (a) J-V characteristic curve of the stretchable PSC at 70% tensile strain. (b) Normalized absorption spectra of stretchable PSCs with and without metal cathode and IPCE of the stretchable PSCs at 70% tensile strain.

The maximal tensile strain of about 70% can be achieved. Random bucklings can be observed clearly. The morphology of the device at 0% strain is intuitively displayed in the SEM image (Fig. 3(b)). The bending radius of the bucklings can be as small as tens of micrometer due to the high flexibility of the ultrathin PSCs.

The current density-voltage (J-V) characteristic of the stretchable PSCs under the maximum tensile strain (nearly planar state) is presented in Fig. 4(a). The device performs with $V_{OC} = 0.9$ V, $J_{SC} = 10.39$ mA cm⁻², FF = 62.0% and PCE = 5.8%. These results are



Fig. 3. (a) Photographs of the stretchable PSCs at 0%, 20%, 50% and 70% tensile strains. (b) Top-view SEM image of the stretchable PSC at 0% tensile strain. The scale bar is 200 µm.

comparable to leading bulk heterojunction (BHJ) PSCs with PCDTBT:PC₇₁BM as absorber and ITO as anode [18]. The UV–visible absorption spectras of devices with and without the metallic cathode and incident photon-to-current efficiency (IPCE) spectra are shown in Fig. 4(b). The absorption spectrum covers entire visible spectral range. An enhancement in absorption >650 nm is observed in the device with the metallic Cathode, which is caused by the microcavity formed by the two metallic electrodes. The peaks in IPCE spectra are consistent well with the absorption spectra of the device without the cathode and the maximum EQE of 68% is achieved.

The I-V characteristics of the stretchable PSCs at different tensile strains are measured and the results are shown in Fig. 5(a). It is clear that the stretchable PSCs can normally work at each tensile strain. With tensile strain increasing, V_{OC} and FF are almost constant, while the short circuit current I_{SC} presents a linear increasing (Fig. 5(b)). This is because the effective light-absorbing area increases linearly with the increasing of the tensile strain.

The stretchable PSCs tend to breakdown during the buckles forming and stretching-releasing process in case the device's cathode contacted directedly with the elastomeric substrate. The cathodes may be damaged by the compressive stress from the elastomer. Here, the 0, 10, 20, 30, 40 nm-thick NPB sacrificial layers were deposited on the cathode films to avoid their contact and improve the mechanical stability of the stretchable PSCs. To investigate the mechanical robustness of the devices, the performance of the stretchable PSCs was measured under the repeated stretching-releasing cycles at tensile strain values between 0% and



Fig. 5. (a) J–V characteristics of the stretchable PSCs at various tensile strains (0%, 15%, 22%, 40%, 56% and 70%). (b) Dependence of the PSC performance on the various tensile strains. All parameters are normalized to their maximum value.



Fig. 6. V_{OC} (a) and I_{SC} (b) vs the stretching cycle number for the stretchable PSCs with 20, 30, 40 nm NPB layer between 0% and 70% strain.

70%. The I-V characteristics at 0% strain were recorded under the solar simulator after every 10 or 20 cycles. The characteristics of V_{OC} and I_{SC} as a function of the cycle number are shown in Fig. 6. In test of cycle stretching, when the thickness of NPB layer was less than or equal to 10 nm, we almost couldn't-test performance of devices and the maximum cycle numbers of the PSCs with 20, 30 and 40 nm NPB layers are 30, 90, and 400, respectively. A thicker sacrificial layer benefits stability of device, while, a thicker layer would result in a poor adhesion between the PSC and the elastomeric substrate. The sacrificial layer of NPB film with 40 nm was chosen in this work. The V_{OC} has almost no change after 400 stretching-releasing cycles. A fluctuation of the lsc can be observed, which is within $\pm 13.2\%$ and may be caused by the fluctuation of the effective area during the stretching-releasing cycles.

4. Conclusions

In summary, we demonstrate stretchable PSCs with high efficiency and improved mechanical robustness based on the random buckling process. A power conversion efficiency of 5.8% under 70% strain has been achieved for the stretchable PSCs, which is by far the highest efficiency among the reported stretchable PSCs. A NPB sacrificial layer was deposited on cathode to avoid direct contact between the PSCs and elastomeric substrate and consequently improve its mechanical robustness. As a result, the stretchable PSCs exhibit small fluctuations in performance after 400 stretchingreleasing cycles. This is an important step towards producing fully stretchable PSCs for applications in wearable electronics.

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